

## A VARIATIONAL DAMAGE MODEL VIA GRADIENT ENHANCEMENT OF THE FREE ENERGY

\* **Bojan J. Dimitrijević<sup>1</sup>** and **Klaus Hackl<sup>2</sup>**

<sup>1</sup> Ruhr-University Bochum  
 Institute of Mechanics  
 Universitätsstrasse 150  
 44801 Bochum, Germany  
 e-mail: Bojan.Dimitrijevic@rub.de  
 URL: <http://www.am.bi.ruhr-uni-bochum.de>

<sup>2</sup> Ruhr-University Bochum  
 Institute of Mechanics  
 Universitätsstrasse 150  
 44801 Bochum, Germany  
 e-mail: Klaus.Hackl@rub.de  
 URL: <http://www.am.bi.ruhr-uni-bochum.de>

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### ABSTRACT

We present a thermoelastic damage model that is based on the gradient-type enhancement of the Helmholtz free-energy function. Direct introduction of the gradient of the damage variable would require  $C^1$  interpolation of the displacements, which is a complicated task to achieve with quadrilateral elements. Therefore an additional variable field  $\varphi$  is introduced (as in [1]), which serves to transport the values of the damage variable across the element boundaries. Besides the gradient term in the non-local variable  $\varphi$ , the modified free energy function includes a term which penalizes the difference between the non-local and local field:

$$\tilde{\psi} = \frac{1}{2} f(d) (\boldsymbol{\epsilon} : \mathbb{C} : \boldsymbol{\epsilon}) + \psi_\theta + \frac{c_d}{2} \|\nabla\varphi\|^2 + \frac{\beta_d}{2} [\varphi - \gamma_1 d]^2 \quad (1)$$

This makes the model non-local in nature, while preserving  $C^0$  interpolation order of the variables at the same time. The price to pay is an additional set of equations which has to be satisfied on the structural level, involving non-local variables and their derivatives. This strategy results in a pure minimization problem, so that the fulfillment of a LBB condition is not an issue to be considered. We take the interpolation of the displacement field one order higher than the interpolation of the field of additional (non-local) variables. That leads to increased accuracy and removes the post-processing step necessary to obtain consistent results in the case of equal interpolation order (see i.e. [2]).

Standard thermodynamic consideration gives as a result driving forces (stress tensor  $\boldsymbol{\sigma}$  and damage conjugate variable  $q$ ). The stress tensor  $\boldsymbol{\sigma}$  maintains the form as in the standard (unenhanced) damage model, while the damage conjugate variable  $q$ , on the other hand, contains contributions from two parts:

$$q := -\frac{\partial\tilde{\psi}}{\partial d} = \underbrace{-\frac{1}{2} f'(d) (\boldsymbol{\epsilon} : \mathbb{C} : \boldsymbol{\epsilon})}_{q_L} + \underbrace{\beta_d \gamma_1 [\varphi - \gamma_1 d]}_{q_{NL}} \quad (2)$$

The first one ( $q_L$ ) originates from the common (local) damage considerations. The second one ( $q_{NL}$ ) reflects the enhancement and is in fact the one that regularizes the model introducing the non-local

influence into the evolution of damage.

The evolution of the damage variable is described following the concept of generalized standard media (as in [3], [4]) through a dissipation potential  $D(\dot{d})$  which depends on the rate of the internal variables and retains its common form:

$$D(\dot{d}) = \sup_q \left[ q\dot{d} - I_K \right] \quad \text{with} \quad I_K(x) = \begin{cases} 0 & \text{if } q \in K \\ +\infty & \text{if } q \notin K \end{cases} \quad (3)$$

The set  $K$  is defined through a convex inelastic constraint (damage threshold condition):

$$K = \{q \mid \phi_d(q) \leq 0\} \quad (4)$$

In the present contribution several numerical examples involving different forms of the damage threshold function  $\phi_d$  will be presented in order to illustrate the performance of the presented gradient enhancement strategy. It is shown that the method efficiently removes pathological mesh dependence together with the numerical difficulties connected with the calculation in the softening range of the materials. Moreover, the influence of the additional model parameters (gradient parameter  $c_d$  and the penalty parameter  $\beta_d$ ) on the global response of the system, distribution of damage and the calculation procedure is discussed. Finally, the extension of the model on other inelastic problems (softening plasticity, combined damage and plasticity), using the same concept, will be presented.

## REFERENCES

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